



# Mono- and bimetallic Rh and Pt NSR-catalysts prepared by controlled deposition of noble metals on support or storage component

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## ARTICLE INFO

### Article history:

Received 5 September 2011

Received in revised form

16 November 2011

Accepted 18 November 2011

Available online 28 November 2011

### Keywords:

Flame spray pyrolysis

NO<sub>x</sub> storage-reduction (NSR)

Mono- and bimetallic catalyst

Platinum

Rhodium

Alumina

Barium carbonate

Selective deposition

Fast NO<sub>x</sub> storage

Lean NO<sub>x</sub> trap

Sulfur poisoning

## ABSTRACT

Mono- and bimetallic Rh and Pt based NO<sub>x</sub> storage-reduction (NSR) catalysts, where the noble metals were deposited on the Al<sub>2</sub>O<sub>3</sub> support or BaCO<sub>3</sub> storage component, have been prepared using a twin flame spray pyrolysis setup. The catalysts were characterized by nitrogen adsorption, CO chemisorption combined with diffuse reflectance infrared Fourier transform spectroscopy, X-ray diffraction, and scanning transmission electron microscopy combined with energy dispersive X-ray spectroscopy. The NSR performance of the catalysts was investigated by fuel lean/rich cycling in the absence and presence of SO<sub>2</sub> (25 ppm) as well as after H<sub>2</sub> desulfation at 750 °C. The performance increased when Rh was located on BaCO<sub>3</sub> enabling good catalyst regeneration during the fuel rich phase. Best performance was observed for bimetallic catalysts where the noble metals were separated, with Pt on Al<sub>2</sub>O<sub>3</sub> and Rh on BaCO<sub>3</sub>. The Rh-containing catalysts generally showed much higher tolerance to SO<sub>2</sub> during fuel rich conditions and lost only little activity during thermal aging at 750 °C.

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## 1. Introduction

Traditional three-way catalysts [1] cannot efficiently reduce NO<sub>x</sub> to N<sub>2</sub> under oxygen rich conditions that are encountered in fuel lean combustion and direct injection engines. Therefore, selective catalytic reduction (SCR) [2] and NO<sub>x</sub> storage-reduction (NSR) catalysts have been developed [3]. In the latter process, the exhaust NO<sub>x</sub> is trapped under oxygen rich conditions on an alkali or alkaline-earth metal (e.g. K, Ba) mainly in the form of corresponding metal nitrates [4]. Because NSR catalysts do not need an additional reducing fuel (like NH<sub>3</sub> or urea as in SCR) and require less mounting space, they are particularly attractive for compact cars [5]. Drawbacks of NSR catalysts are connected with deterioration [6], thermal aging [7] and sulfur poisoning [8]. Sulfur typically present in the fuel and lubricant oils [9] is oxidized to SO<sub>2</sub> during combustion. The SO<sub>2</sub> in the exhaust gas can adsorb on the catalyst and poison it. As-poisoned catalysts typically require regeneration temperatures above 700 °C [10]. Catalyst deactivation was found to be strongest

by SO<sub>2</sub>, compared to other sulfur-containing species like H<sub>2</sub>S and COS [11]. Furthermore, SO<sub>2</sub> deactivates NSR catalysts faster during the fuel rich periods [12].

The effect of SO<sub>2</sub> on the storage component and the noble metal are different [12]: As concerns the noble metal, SO<sub>2</sub> can have negative as well as positive influence on the catalyst's oxidation activity e.g. while 20 ppm SO<sub>2</sub> decreased the activity for propene oxidation of Pt/Al<sub>2</sub>O<sub>3</sub> catalysts, the same concentration of SO<sub>2</sub> had a positive effect on propane oxidation [13] because PtO<sub>2</sub> is reduced in the presence of SO<sub>2</sub> to Pt [14]. In contrast to Pt, for Rh no loss of NO reduction activity was observed in the presence of SO<sub>2</sub> [15]. Furthermore Rh is a highly active NO reduction catalyst [16] that enhances the regeneration of Ba-nitrates [17]. After regeneration of H<sub>2</sub>S poisoned catalysts, Rh showed the highest CH<sub>4</sub> oxidation performance among alumina supported Pt, Pd or Rh catalysts [18]. In the presence of SO<sub>2</sub>, the NO<sub>x</sub> reduction activity of Pt based catalysts decreases while that of Rh catalysts is less affected [19]. For Rh, however, the NO<sub>x</sub> oxidation is inhibited in the presence of SO<sub>2</sub>, while Pt shows considerable tolerance [20]. Combinations of Pt and Rh maintained their activity for the entire NSR process [21]. Also for CO/hydrocarbon mixtures, combinations of Pt and Rh gave better performance than either metal alone [22]. Computational analysis

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predicted the segregation of Rh to the surface of Pt for combined Rh/Pt systems [23].

Sulfur compounds can also chemisorb on the storage component finally forming sulfates [24], e.g. BaSO<sub>4</sub> which decomposes at higher temperatures than Ba(NO<sub>3</sub>)<sub>2</sub> and thus lowers the number of Ba-sites active in NO<sub>x</sub> storage. The rate of NO<sub>x</sub> uptake was found to decrease proportionally to the SO<sub>2</sub> dosing, indicating that the amount of SO<sub>2</sub> uptake is more important than the actual SO<sub>2</sub> concentration for catalyst deactivation [25].

With flame spray pyrolysis (FSP) a variety of materials for different catalytic applications have been synthesized [26]. For NSR catalysts, a two-nozzle FSP setup was used to produce the Ba and Al components separately [27]. The as-formed BaCO<sub>3</sub> is finely dispersed on the support and can decompose to BaO and CO<sub>2</sub> below 600 °C [28]. Additionally, the two-nozzle FSP allows preferential deposition of noble metals on the storage or support components [29]. Also bimetallic Pt/Pd clusters were produced with FSP [30]. These bimetallic systems were more stable at higher temperature (1000 °C) [31] than corresponding monometallic ones, and had higher sulfur tolerance [32] and oxidation activity [33]. It was shown previously that the location of the noble metal is important in NSR: While Pt on Al<sub>2</sub>O<sub>3</sub> showed a high NO oxidation activity [34], Pt on the Ba component showed a tendency to form PtO<sub>x</sub> which is less active than Pt<sup>0</sup> for NO oxidation [35]. Nevertheless, Pt on the Ba component also promotes Ba(NO<sub>3</sub>)<sub>2</sub> decomposition leading to good regeneration of the Ba storage component and long cycle life [36].

Here, we investigated the structural and catalytic properties of mono- and bimetallic Rh and Pt based NSR catalysts where the noble metals were preferentially deposited either on the alumina support or on the storage component (BaCO<sub>3</sub>). The influence of the noble metals and their location on the NSR performance was investigated in the absence and presence of SO<sub>2</sub> in the feed gas.

## 2. Experimental

Mono- and bimetallic alumina-supported Rh and Pt catalysts containing BaCO<sub>3</sub> as storage component were prepared using a two-nozzle FSP [27] unit with a two-nozzle angle of 160° to ensure the preferential deposition of noble metals [29]. Each nozzle used a premixed CH<sub>4</sub>/O<sub>2</sub> flame at a volume ratio of 1/2 to ignite and sustain the spray [37]. The Al-precursor solution consisted of aluminum-tri-sec-butoxide (Fluka, 95%) dissolved in a 2:1 vol. ratio of diethylene glycol monobutyl ether (Fluka, 98%) and acetic anhydride (Riedel-de Haën, 99%). The aluminum concentration was kept constant at 0.5 mol/L. The Ba-precursor solution consisted of barium 2-ethylhexanoate (Aldrich, 98%) dissolved in 1:1 vol ratio of toluene (Riedel-de Haën, 99%) and 2-ethylhexanoic acid (Riedel-de Haën, 95%) for a Ba concentration of 0.06 mol/L. Appropriate amounts of Rh(III)-acetylacetone (Sigma-Aldrich, 99.99%) and/or platinum(II) acetylacetone (Alfa Aesar, 98%) were added either to the Ba- or Al-solutions. The Ba- and Al-precursor solutions were sprayed at 3 and 5 ml/min, respectively, and both were dispersed with 5 L/min O<sub>2</sub> (Pangas, 99.95%) each. The Al-, Ba-, Rh/Pt-concentration and spray rates were chosen to result in a nominal (Rh + Pt)/Ba/Al<sub>2</sub>O<sub>3</sub> weight ratio of 1/20/100. This corresponds to a noble metal weight loading of 0.78 wt%, assuming that all Ba is present as BaCO<sub>3</sub> [28]. Note that the flame made catalysts were not subject to an additional temperature pretreatment as usually applied for conventionally prepared catalysts.

In the notation used here, the noble metal and its mass relative to the support are written next to the material with which it was co-produced, and therefore preferential deposition on these components is expected [36]. For example, 0.5PtAl-Ba0.5Rh means that Pt-acetylacetone was dissolved in the Al-precursor

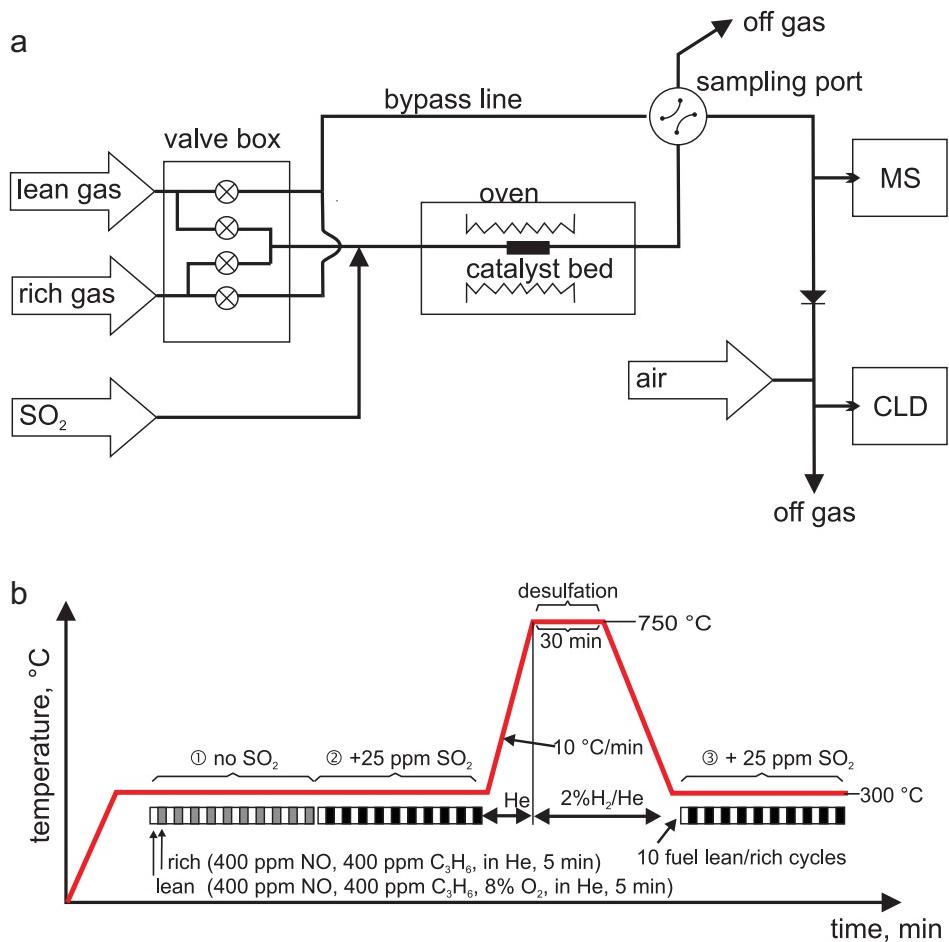
solution and Rh-acetylacetone was dissolved in the Ba-precursor solution with a weight ratio of Rh/Pt/Ba/Al<sub>2</sub>O<sub>3</sub> of 0.5/0.5/20/100. With bimetallic catalysts we distinguish between “separated” and “mixed” catalysts. In the former the two metals were deposited on different constituents (support, storage), in the latter the two metals were deposited without preferential deposition. For comparison a Pt/Ba/Al<sub>2</sub>O<sub>3</sub> reference catalyst was prepared by means of wet-impregnation according to the procedure reported in [38].

Nitrogen adsorption–desorption isotherms were measured at 77 K using a Micromeritics Tristar instrument. The BET method was used to determine the specific surface area (SSA) by a 5-point nitrogen adsorption isotherm. The estimated accuracy is ±3%. X-ray diffraction (XRD) patterns were recorded with a Bruker D8 Advance instrument (40 kV, 40 mA,  $\lambda = 0.154$  nm). Crystallite sizes and mass fractions were calculated using the fundamental parameter approach and the Rietveld method with the TOPAS 3 software at ±10% accuracy [36].

For scanning transmission electron microscopy (STEM), the catalyst material was dispersed in ethanol and deposited onto a perforated carbon foil supported on a copper grid (Okenshoji Co. Ltd.). The STEM images were obtained with a high-angle annular dark-field (HAADF) detector attached to a Tecnai 30F microscope (FEI; field emission cathode, operated at 300 kV), showing the metal particles with bright contrast (Z contrast). For qualitative analysis, the electron beam was set to selected areas in the STEM images and the signal was measured by energy dispersive X-ray spectroscopy (EDXS; detector: EDAX).

The amount of CO chemisorbed on the noble metals was measured using a Micromeritics Autochem II 2920 with 10 CO-pulses at 40 °C after pretreating the catalysts at 300 °C under 5% H<sub>2</sub>/Ar [28]. Diffuse reflectance infrared Fourier transform spectroscopy (DRIFTS) was carried out with a VECTOR 22 spectrometer (Bruker Optics). Spectra were obtained by averaging 100 scans at 4 cm<sup>-1</sup> resolution. The average stoichiometric factor (SF) of chemisorbed CO was determined by taking the ratio from the peak area between linear and bridged bonded CO [39] of the spectrum at ±5% accuracy. Band positions below 1950 cm<sup>-1</sup> were considered as bridged bound CO, while linear bound CO is that between 2100 cm<sup>-1</sup> and 1950 cm<sup>-1</sup> [40]. A sensitivity ratio of 0.8 for bridged CO with respect to linear bond CO was assumed based on previous DFT simulations [41]. The average noble metal dispersion (%) was calculated from the specific CO uptake mol<sub>CO</sub>/mol<sub>metal</sub> multiplied with the corresponding average stoichiometric factor (SF) determined by DRIFTS.

For NSR testing, the as prepared powder was pelletized (5.9 kg/mm<sup>2</sup>), ground and sieved: 20 mg of catalyst with 0.08–0.14 mm size fraction were mixed with inert 383 mg SiC (size fraction 0.18–0.24 mm) and was placed in a quartz glass reactor with an inner diameter of 4 mm, resulting in a catalyst bed length of 2 cm. The time to equilibrate between lean and rich mixtures (measured with inert SiC materials) was approximately 90 s. The as-prepared catalyst was heated up to 300 °C under 300 mL/min He. A schematic of the reactor setup and the experimental procedure applied for the catalytic tests is shown in Fig. 1. With mass flow controllers (Brooks, 5850S) the O<sub>2</sub> (Pangas, 99.95%), C<sub>3</sub>H<sub>6</sub> (Pangas, 1% in He), NO (Linde, 1% in He) and He (Pangas, 99.996%) were mixed to a total of 500 mL/min (assuming a void space of 0.4 this results in a space velocity of 300,000 h<sup>-1</sup>) of fuel lean (400 ppm NO, 500 ppm C<sub>3</sub>H<sub>6</sub>, and 8% O<sub>2</sub>, balance He), and fuel rich gases (400 ppm NO and 500 ppm C<sub>3</sub>H<sub>6</sub>, balance He), similar to Ambergsson et al. [21]. Note that this space velocity is considerably higher than the space velocities often used in model type studies which range between 10,000 and 120,000 h<sup>-1</sup> [42,43]. We have used this high space velocity because it allowed a better discrimination between the performances of the different catalysts. Furthermore it is interesting to explore the catalytic performances at higher space velocity because these experiments give a rough idea where the limitations



**Fig. 1.** Scheme of experimental setup (a) and procedure applied in catalytic tests (b).

with regard to the compacting of catalytic converters are. For comparison some experiments were also carried out at a lower space velocity of 38,000 h<sup>-1</sup>. With six control valves, the feed was controlled in a way that either fuel lean or rich gas flowed through the catalyst bed, while the other gases were flowing through the by-pass line to the sampling port.

The horizontally oriented oven (HTM Reetz, LK1100-40-400-2) allowed to heat the catalyst up to 1100 °C. All gas lines (stainless steel) were heated to 120 °C to prevent water condensation. At the sampling port either the catalyst off-gas or the gas from the bypass line was selected to calibrate the inlet concentration. The off-gas was analyzed with a quadrupol mass spectrometer (MS; Pfeiffer vacuum, ThermoStar GSD 301) and a chemiluminescence detector (CLD; ECO Physics, CLD 822S). Before the CLD, the off-gas was diluted with 400 mL/min air. Previously fast FTIR analysis for experiments with similar materials showed no formation of NH<sub>3</sub>, and N<sub>2</sub>O only for short periods of about 20 s when switching from fuel rich to fuel lean conditions [44].

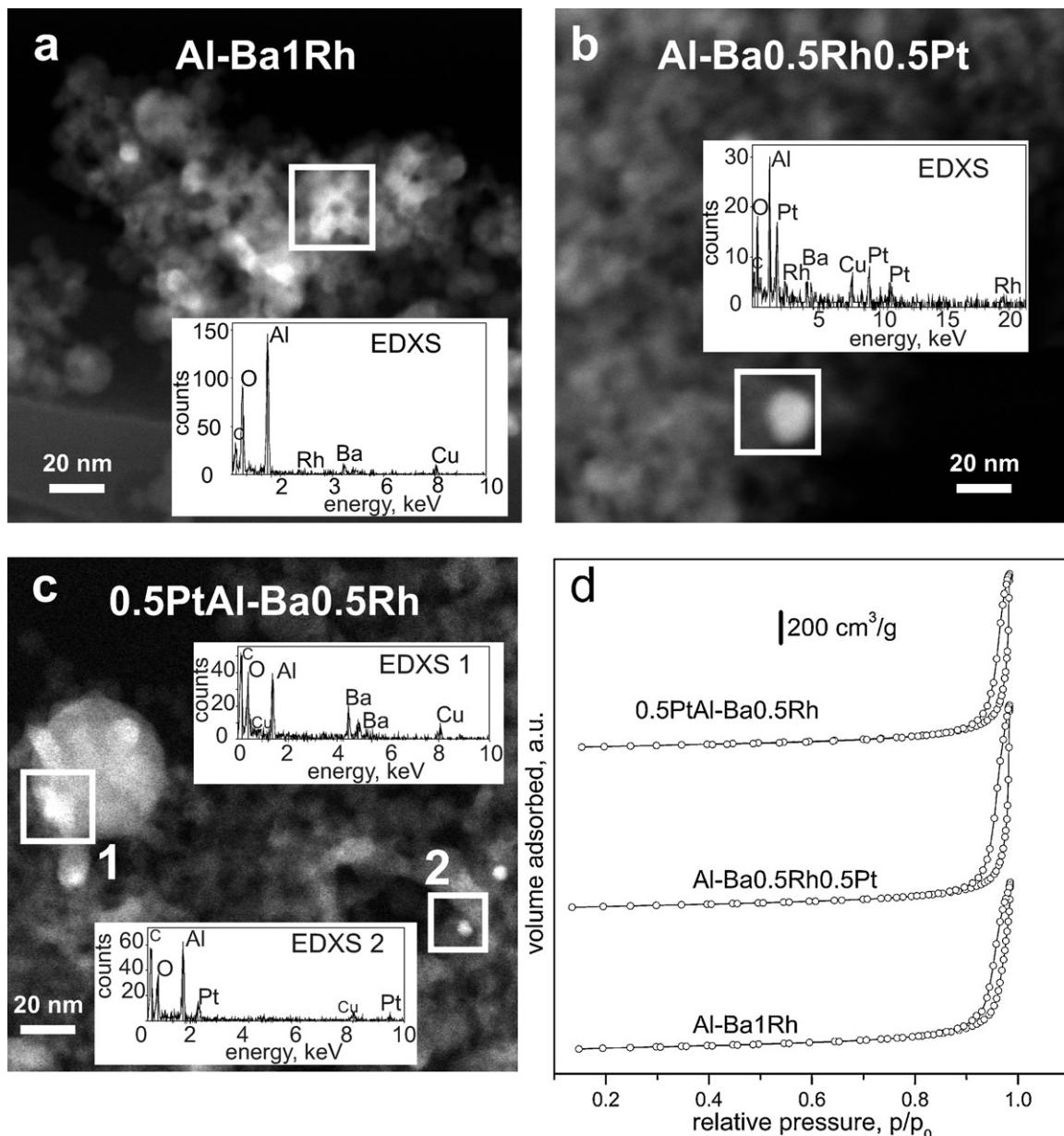
The catalyst test procedure is illustrated in Fig. 1b. Catalytic performance was tested first for 10 cycles without sulfur dioxide, then for 10 cycles with 25 ppm SO<sub>2</sub> (2.5 mL/min, 5000 ppm SO<sub>2</sub> in N<sub>2</sub>, Pangas) while each cycle exposed the catalysts 5 min to a fuel lean and 5 min to a fuel rich gas composition. Note that these cycling periods were chosen due to some constraints given by the experimental setup used. The catalyst was then heated to 750 °C at 10 °C/min under 500 mL/min He and then held isothermally at this temperature for 30 min. There, the catalyst was reduced with 2% H<sub>2</sub> in He (500 mL/min) and cooled down to 300 °C where the

catalyst was tested again for 10 fuel lean/rich cycles in the presence of 25 ppm SO<sub>2</sub>. For each cycle the integral NO<sub>x</sub> conversion for each cycle was calculated as: NO<sub>x,conv</sub> = (NO<sub>x,in</sub> - NO<sub>x,out</sub>) / NO<sub>x,in</sub>. When repeating measurement with fresh material the reported values varied by less than 10%. The stored NO<sub>x</sub> was calculated by integration of the NO<sub>x</sub> stored on the catalyst during the fuel lean phase. The reported values are representative values, after the storage and reduction cycles reached steady-state: the durations of the different measurement series 1–3 were: 1) 40–50 min (without SO<sub>2</sub>), 2) 160–170 min (with 25 ppm SO<sub>2</sub>), and 3) 472–482 min (with SO<sub>2</sub>, after desulfation). The estimated accuracy was ±5%. In order to account for possible NO<sub>x</sub> uptake and conversion caused by the experimental setup, blind tests with inert material (SiC) were performed. These blind tests indicated NO<sub>x</sub> consumption of <4% which has been taken into account in the data evaluation. Complete saturation experiments were performed under the same gas flow conditions but the cycle length was extended to 2 h (1 h lean and 1 h rich) and the cycles were repeated 4 times without SO<sub>2</sub> followed by 3 cycles in the presence of 25 ppm SO<sub>2</sub>. All gas flows were calibrated to 0 °C (Bios, Definer 220) with an accuracy of ±1%.

### 3. Results and discussion

#### 3.1. Structural properties of catalysts

Four types of M/BaCO<sub>3</sub>/Al<sub>2</sub>O<sub>3</sub> NSR catalysts with different noble metal (M) composition were synthesized using the twin nozzle system: Monometallic Rh and Pt catalysts as well as bimetallic mixed



**Fig. 2.** STEM and EDXS of indicated area for selected catalysts (a). Al-Ba1Rh, (b) Al-Ba0.5Rh0.5Pt, and (c) 0.5PtAl-Ba0.5Rh. The Cu signal in the EDXS is due the support grid. In (d) BET isotherms of these particles are shown, indicating that they are non-porous.

Rh/Pt, and *separated* Rh and Pt catalysts. In *mixed* Rh/Pt catalysts both noble metal precursors were fed through the same nozzle resulting in their deposition on both the support ( $\gamma\text{-Al}_2\text{O}_3$ ) and storage component ( $\text{BaCO}_3$ ). In *separated* Rh and Pt catalysts one noble metal was deposited on the support and the other on the storage material. We have demonstrated in a previous study by means of electron microscopy combined with EDX [36] that the twin nozzle system applied for the synthesis of the catalysts effectively allows the preferential deposition of noble metal particles on either the storage or support material. Here we used DRIFTS measurement with CO to estimate approximate mean stoichiometric factors of the CO adsorption and to gain some information about the oxidation state of the noble metals.

Fig. 2a–c shows for selected catalysts the typical STEM images with EDXS of the highlighted area. The Rh signal in EDXS was difficult to detect as seen for Al-Ba1Rh (Fig. 2a) probably due to the lower X-ray yield of Rh ( $Z=45$ ) compared to Ba ( $Z=56$ ) and Pt ( $Z=78$ ). Only in bimetallic *mixed* Al-Ba0.5Pt0.5Rh (Fig. 2b)

simultaneously Rh and Pt were detected. In the bimetallic *separated* 0.5PtAl-Ba0.5Rh (Fig. 2c) the Ba and Pt were not detected together as expected for preferential deposition. The Cu and part of the C signal are due to the Cu containing grid. All the flame-derived catalyst powders were virtually nonporous as indicated by the typical nitrogen adsorption-desorption isotherms observed (Fig. 2d), which all showed a hysteresis at high relative pressure due to the interparticle void space of the powders.

Some properties (BET surface areas,  $\text{BaCO}_3$  and  $\text{Al}_2\text{O}_3$  crystallite sizes, CO adsorption uptake, stoichiometric factors of CO adsorption and average metal dispersion) of the flame derived catalysts are listed in Table 1. The surface area (SSA) for Rh-containing catalysts was fairly constant ( $161\text{--}170 \text{ m}^2/\text{g}$ ). The Pt-only catalysts showed a slightly lower SSA ( $124\text{--}137 \text{ m}^2/\text{g}$ ). This may be attributed to the fact that the total noble metal weight was fixed to 0.78 wt% resulting in almost two times higher number of Rh than Pt atoms due to the much lower atomic weight of the former ( $A_{\text{Rh}} = 102.9 \text{ g/mol}$ , compared to Pt ( $A_{\text{Pt}} = 195.1 \text{ g/mol}$ )). Interestingly, a similar

**Table 1**

Structural properties of flame-made catalysts. Specific surface area (SSA), specific CO uptake, average stoichiometric factor (SF), and noble metal dispersion.

|                     | Catalyst        | SSA <sup>a</sup> (m <sup>2</sup> /g) | $d_{\text{BaCO}_3}$ <sup>b</sup> (nm) | $d_{\text{Al}_2\text{O}_3}$ <sup>c</sup> (nm) | CO adsorption (mol <sub>CO</sub> /mol <sub>(Rh+Pt)</sub> ) | SF <sup>d</sup> | Dispersion (%) |
|---------------------|-----------------|--------------------------------------|---------------------------------------|---|--|-----------------|----------------|
| <b>Monometallic</b> |                 |                                      |                                       |   |  |                 |                |
| Rh-only             | 1RhAl-Ba        | 161                                  | 8                                     | 9   | 0.23   | 1.01            | 23             |
|                     | Al-Ba1Rh        | 163                                  | 5                                     | 12  | 0.06   | 1.17            | 6              |
| Pt-only             | 1PtAl-Ba        | 124                                  | 8                                     | 10  | 0.24   | 1.16            | 24             |
|                     | Al-Ba1Pt        | 137                                  | 7                                     | 12  | 0.22   | 1.30            | 22             |
| <b>Bimetallic</b>   |                 |                                      |                                       |   |  |                 |                |
| Mixed Rh/Pt         | 0.5Rh0.5PtAl-Ba | 170                                  | 8                                     | 10  | 0.24   | 1.04            | 24             |
|                     | Al-Ba0.5Rh0.5Pt | 163                                  | 6                                     | 9   | 0.10   | 1.13            | 10             |
| Separated Rh and Pt | 0.5RhAl-Ba0.5Pt | 170                                  | 8                                     | 8   | 0.36   | 1.25            | 36             |
|                     | 0.5PtAl-Ba0.5Rh | 167                                  | 7                                     | 9   | 0.15   | 1.22            | 15             |

<sup>a</sup> Specific surface area (SSA) measured with BET method.

<sup>b</sup> Mean crystallite size of as prepared BaCO<sub>3</sub> by X-ray line broadening of (111) monoclinic BaCO<sub>3</sub>.

<sup>c</sup> Mean crystallite size of Al<sub>2</sub>O<sub>3</sub> determined by X-ray line broadening of (224) reflections.

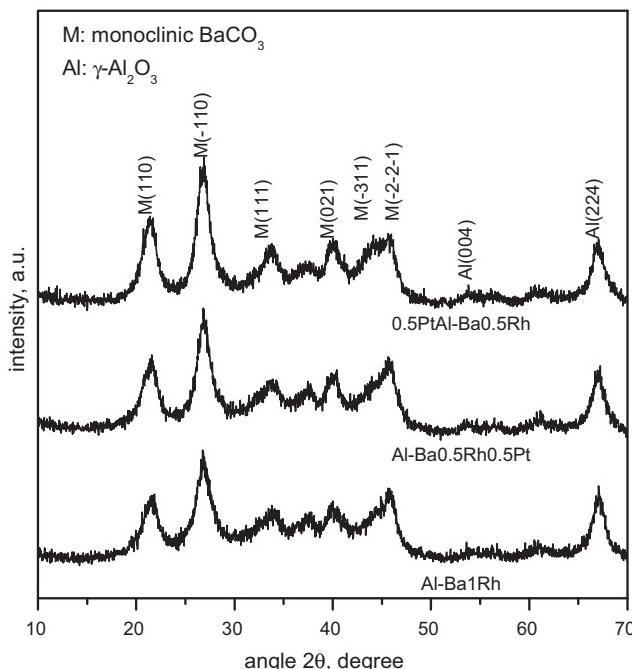
<sup>d</sup> Stoichiometric factor (SF) determined from DRIFT measurements and used to calculate the noble metal dispersion.

contribution to the surface area was not observed with correspondingly prepared Pd ( $A_{\text{Pd}} = 106.4 \text{ g/mol}$ ) catalysts [30] which showed about the same SSA ( $130 \text{ m}^2/\text{g}$ ) as the Pt catalysts. Corresponding flame-made pure  $\gamma$ -Al<sub>2</sub>O<sub>3</sub> and BaCO<sub>3</sub> showed SSAs of  $148 \text{ m}^2/\text{g}$  and  $20 \text{ m}^2/\text{g}$ , respectively [36].

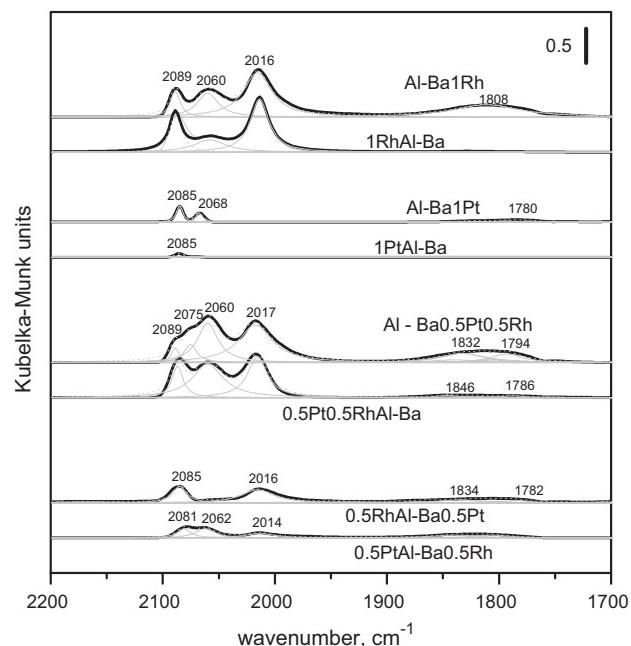
The bulk structure of as-prepared catalysts was determined by powder XRD (Fig. 3). Fresh as-prepared powders showed the monoclinic BaCO<sub>3</sub> phase that transforms after some days, into the more stable orthorhombic BaCO<sub>3</sub> [45]. The reported crystallite sizes of BaCO<sub>3</sub> refer to as-prepared powders, where no orthorhombic BaCO<sub>3</sub> was observed. Mean crystallite sizes derived from X-ray line broadening for the storage and support components were (Table 1): BaCO<sub>3</sub>, 5–8 nm; Al<sub>2</sub>O<sub>3</sub>, 8–12 nm.

CO adsorption measurements clearly showed higher CO uptake for catalysts where Rh was deposited on alumina, while Rh deposition on BaCO<sub>3</sub> resulted in low CO uptake indicating low dispersion. This is attributed to both the higher specific surface area of Al<sub>2</sub>O<sub>3</sub> compared to BaCO<sub>3</sub> as well as the difference in surface properties between these materials e.g. the acid-base properties and wetting angle [46]. The noble metal dispersion ranged from 6% (Al-Ba1Rh) to 36% (0.5RhAl-Ba0.5Pt).

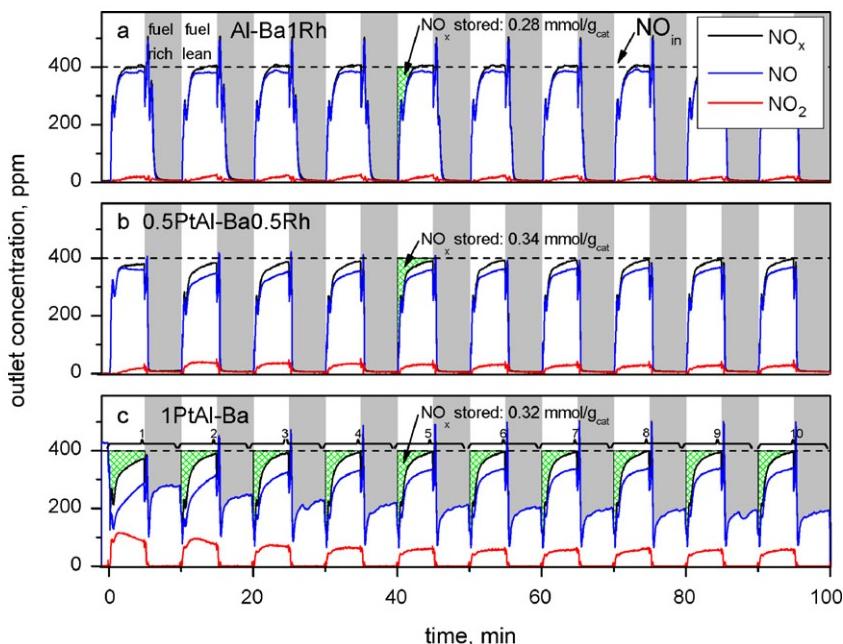
DRIFTS measurements of CO adsorption (Fig. 4) provided further insight into the state of the noble metals present in the flame-derived catalysts. As regards the spectra intensities, similar signal intensity for comparable materials were observed with the exception of the Pt-only catalysts showing a three times lower signal intensity. The higher intensity of the vibrational bands observed with Rh-only catalysts reflects the higher amount of CO chemisorbed. For chemisorbed CO on Rh, three vibrational modes have been identified: dicarbonyl species at  $2104 \text{ cm}^{-1}$ , linear-bonded CO at around  $2034 \text{ cm}^{-1}$  and bridged CO at  $1870 \text{ cm}^{-1}$  [39]. In Fig. 4 all signals have their maximum below  $2100 \text{ cm}^{-1}$  and therefore the presence of dicarbonyl adsorption on Rh can be neglected, typically assigned to extremely small Rh clusters (<1 nm) or atomically dispersed Rh<sup>1+</sup> sites [47]. Linear and bridged CO can be associated with CO adsorption on crystalline Rh sites [39]. Similar assignments have been found also for CO-Pt bonding [48]. The DRIFT spectra in Fig. 4 show the typical linear CO bonding at around  $2080 \text{ cm}^{-1}$  and a broad band at  $1800 \text{ cm}^{-1}$  assigned to bridged CO. From the areas below linear and bridged CO, the average stoichiometric factors (SFs) were calculated (Table 1).



**Fig. 3.** XRD patterns of selected as-prepared catalysts. Characteristic reflections of monoclinic BaCO<sub>3</sub> (ICSD: 63257) and Al<sub>2</sub>O<sub>3</sub> (ICSD: 99836) are indicated.



**Fig. 4.** DRIFT spectra of CO adsorption and the deconvoluted components of the CO bands for Rh and/or Pt deposited on Al<sub>2</sub>O<sub>3</sub> or BaCO<sub>3</sub>. The deconvoluted components are represented with dashed and gray lines, respectively.



**Fig. 5.** Reactor outlet concentrations of  $\text{NO}_x$  (NO,  $\text{NO}_2$ ) without sulfur dosing for selected catalysts: (a) Al-Ba1Rh (b) 0.5PtAl-Ba0.5Rh and (c) 1PtAl-Ba. While (a) and (b) stored  $\text{NO}_x$  under fuel lean conditions, (c) PtAl-Ba had difficulties to reduce  $\text{NO}_x$  under fuel rich conditions. The cycles are numbered 1–10 and the fuel lean/rich periods are illustrated in (a). The stored  $\text{NO}_x$  equivalent area is highlighted. Conditions: fuel lean period: 400 ppm NO, 500 ppm  $\text{C}_3\text{H}_8$ , and 8%  $\text{O}_2$ , balance He. Fuel rich period: 400 ppm NO and 500 ppm  $\text{C}_3\text{H}_8$ , balance He. Both at 300 °C and space velocity of 300,000  $\text{h}^{-1}$ .

Basic surfaces increase the ratio of bridged to linear bonded CO [49] caused by the increase of the electron density of the noble metal [50]. Therefore noble metals deposited on  $\text{BaCO}_3$  had higher SFs than those on  $\text{Al}_2\text{O}_3$ . This trend can be seen in Table 1 for: Rh-only ( $1\text{RhAl-Ba}$ , SF = 1.01 <  $\text{Al-Ba1Rh}$ , SF = 1.17), Pt-only ( $1\text{PtAl-Ba}$ , SF = 1.16 <  $\text{Al-Ba1Pt}$ , SF = 1.30) and even for the *mixed* Rh/Pt catalysts ( $0.5\text{Rh}0.5\text{PtAl-Ba}$ , SF = 1.04 <  $\text{Al-Ba0.5Pt0.5Rh}$ , SF = 1.13). For separated Rh and Pt both SFs were in the same order (1.25 and 1.22).

As will be shown later in Section 3.2, the metal dispersion alone was not the main factor determining the catalysts' activity. The location of noble metal on the catalysts was found to be even more crucial for efficient NO oxidation and reduction.

### 3.2. Catalytic behavior

The catalytic tests aimed at elucidating the influence of the controlled deposition of the noble metals (Pt, Rh) on the storage and support constituents on the NSR performance of the flame-made catalysts. For this purpose the catalytic behavior was investigated in the absence and presence of  $\text{SO}_2$  in the feed.

#### 3.2.1. Sulfur-free $\text{NO}_x$ storage and reduction

In Fig. 5 the outlet  $\text{NO}_x$  concentrations for three selected catalysts<sup>1</sup> are compared during the first ten sulfur-free cycles. At the positions where conditions are changed from lean to rich cycles, a  $\text{NO}_x$  breakthrough peak appeared in all cycling experiments. The intensity of this breakthrough peak depended on the catalyst type. The small spikes observed at the change from rich to lean conditions are due to an apparatus artifact caused by the switching as blind tests revealed.

Among the three catalysts shown in Fig. 5, 0.5PtAl-Ba0.5Rh (Fig. 5b) showed the highest  $\text{NO}_x$  storage capacity (0.34 mmol/g) and overall NSR performance followed by 1PtAl-Ba (Fig. 5c)

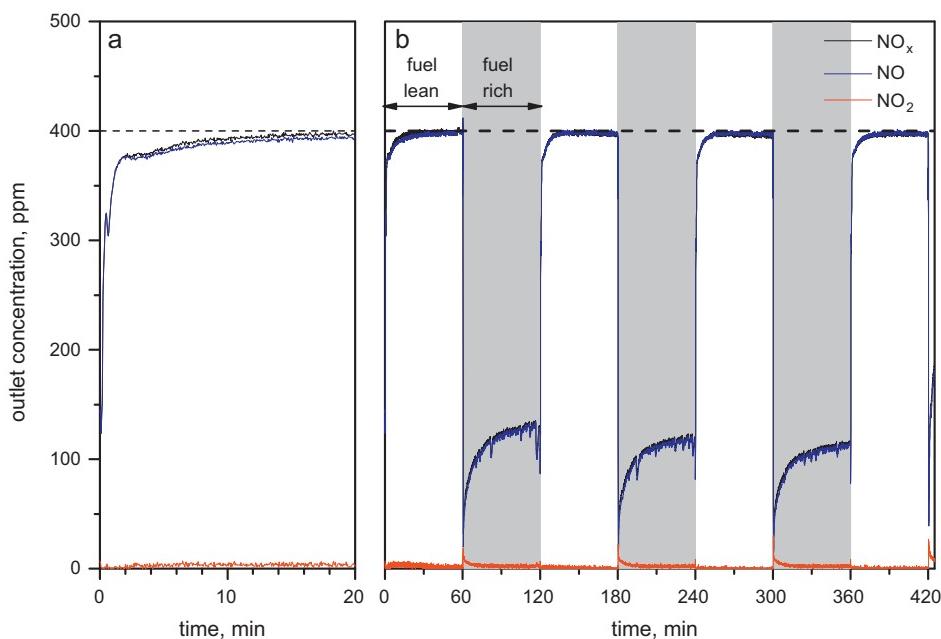
(0.32 mmol/g) and Al-Ba1Rh (0.28 mmol/g (Fig. 5a)). Note that the storage material was regenerated to the same level after each cycle, showing constant storage capacity. The storage capacity did not significantly vary depending on the noble metal or its preferential deposition, as the Ba-loading was the same for all catalysts investigated and the storage time was chosen long enough to reach an uptake close to saturation as will be shown later in Fig. 6. While during the lean cycle virtually no  $\text{NO}_2$  was observed with Al-Ba1Rh, and only little with 0.5PtAl-Ba0.5Rh, 1PtAl-Ba showed significant amount of  $\text{NO}_2$ . The behavior is attributed to the high NO oxidation activity of Pt combined with a less efficient regeneration of the storage component ( $\text{BaCO}_3$ ) during the rich phase. Similar behavior was observed for Pt/Ba/ $\text{Al}_2\text{O}_3$  and Pt-Rh/Ba/ $\text{Al}_2\text{O}_3$  catalysts by Amberntsson et al. [21], although the  $\text{NO}_x$  concentration was lower (100 ppm) and experiments were performed at higher temperature (400 °C) and lower space velocity (38,000  $\text{h}^{-1}$ ).

In order to gain further information on the storage and reduction behavior, the best catalyst of this series (0.5PtAl-Ba0.5Rh) was exposed to 1 h lean and 1 h rich cycles (Fig. 6b). Complete  $\text{NO}_x$  saturation was observed after about 20 min (Fig. 6a). The  $\text{NO}_x$  uptake rate decreased with time, as saturation was approached. Fast uptake in the beginning is attributed to formation of surface nitrates, while in a later stage  $\text{NO}_x$  has to diffuse into the bulk of the storage component [51]. During the fuel rich phase in Fig. 6b all  $\text{NO}_x$  is reduced during the first minutes, however,  $\text{NO}_x$  concentration increases with time probably due to a reversible self poisoning of the noble metal [53] with oxygen from the NO [52]. The substantial outlet concentration of  $\text{NO}_x$  during the rich period is a consequence of the very high space velocity used. From Fig. 6 it can be concluded that the choice of much shorter lean-rich cycling periods would probably be advantageous when using such a high space velocity. Proper adjustment of both cycling periods as well as space velocity is essential for optimal catalyst performance.

#### 3.2.2. $\text{NO}_x$ storage and reduction in the presence of $\text{SO}_2$

After the first ten sulfur-free cycles (Fig. 5), 25 ppm  $\text{SO}_2$  was dosed to the inlet gas (5 min fuel lean and 5 min fuel rich conditions). Fig. 7 shows the  $\text{NO}_x$  outlet concentration for selected

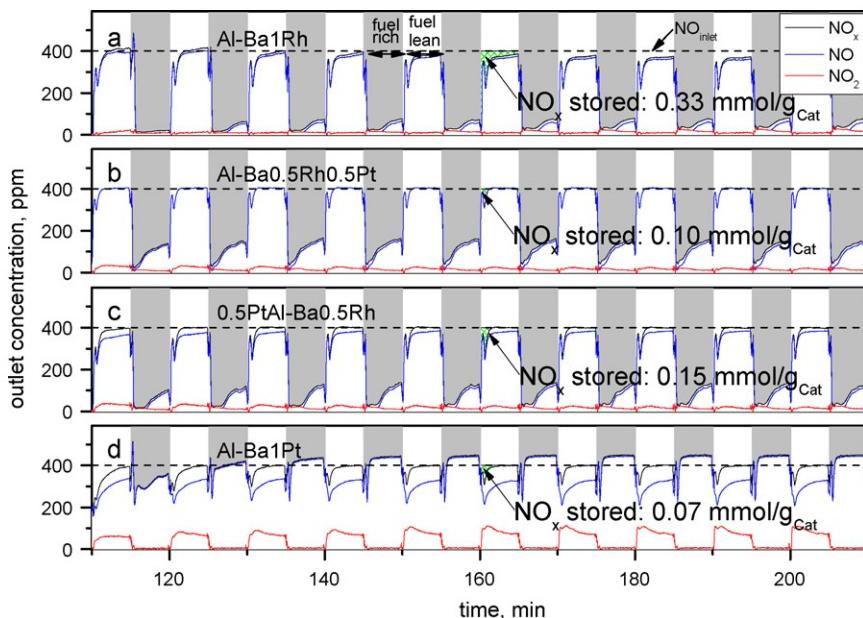
<sup>1</sup> Later on we will show that the bimetallic 0.5PtAl-Ba0.5Rh is the best among the tested catalyst, therefore it is here compared to the monometallic Al-Ba1Rh and 1PtAl-Ba.



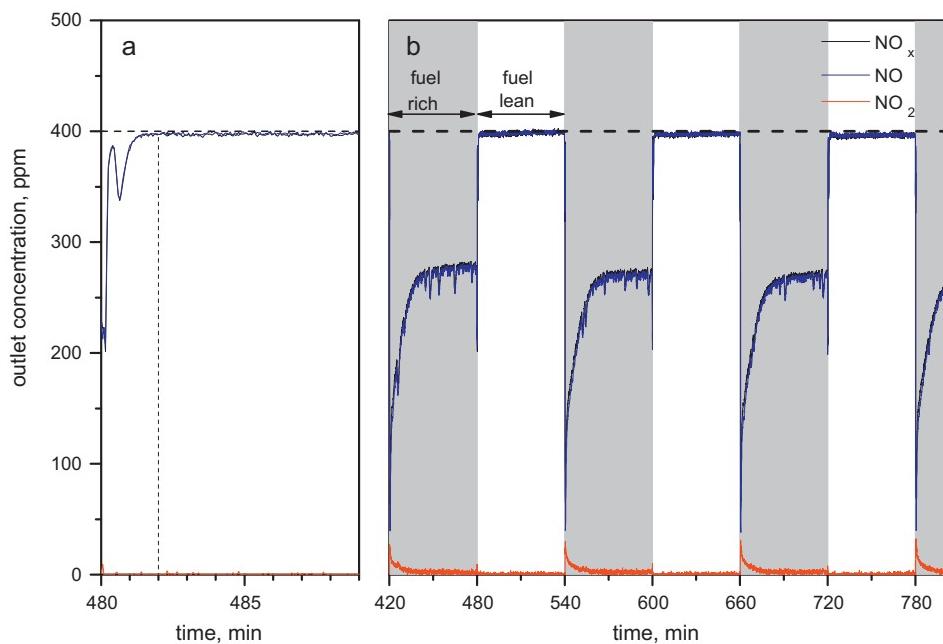
**Fig. 6.** Complete storage and reduction of 0.5PtAl-Ba0.5Rh catalysts in the absence of SO<sub>2</sub>. (a) First 20 min of fuel lean cycle, (b) first 4 cycles. Conditions: fuel lean period: 400 ppm NO, 500 ppm C<sub>3</sub>H<sub>6</sub>, and 8% O<sub>2</sub>, balance He. Fuel rich period: 400 ppm NO and 500 ppm C<sub>3</sub>H<sub>6</sub>, balance He. Both at 300 °C and space velocity of 300,000 h<sup>-1</sup>.

catalysts. For Al-Ba1Rh (Fig. 7a) the first fuel lean/rich cycle was not affected by the presence of SO<sub>2</sub>, and almost no NO<sub>x</sub> was emitted during the fuel rich phase. During the second and third cycle, the NO<sub>x</sub> emission during the fuel rich conditions increased, becoming constant at about 60 ppm (Fig. 7a). During fuel rich conditions, NO<sub>x</sub>, from the engine off-gas, can be converted directly according to the three-way catalyst principle. Furthermore the saturated storage sites (here Ba(NO<sub>3</sub>)<sub>2</sub>) must be regenerated (to BaCO<sub>3</sub> or BaO) to store NO<sub>x</sub> during the subsequent fuel lean cycle. If the Ba component is not regenerated properly, the storage capacity is lost very quickly as observed for Al-Ba1Pt, where after addition of 25 ppm SO<sub>2</sub> almost no NO<sub>x</sub> (0.07 mmol/g<sub>cat</sub>, Fig. 7d) is stored anymore.

Note that in Fig. 7d the NO<sub>x</sub> concentration during the fuel rich condition is higher than the actual 400 ppm NO<sub>x</sub> inlet concentration, which is an artifact caused by the analytical system (CLD), where the gas is sampled based on pressure difference through a critical orifice. The indicated NO<sub>x</sub> signal during the fuel rich condition is therefore higher than the actual NO<sub>x</sub> concentration. Note that the underestimation of the NO<sub>x</sub> conversion was maximal 5%. The NO<sub>x</sub> reduction activity during the fuel rich cycle is very important for sustaining the overall NSR performance. When the regeneration (reduction/decomposition) of the stored NO<sub>x</sub> is insufficient less NO<sub>x</sub> can be stored during the subsequent fuel lean cycle. The NO<sub>x</sub> storage capacity increased from 0.28 mmol/g<sub>cat</sub> (Fig. 5a) to 0.33 mmol/g<sub>cat</sub>



**Fig. 7.** Reactor outlet concentration of NO<sub>x</sub> (NO, NO<sub>2</sub>) with 25 ppm SO<sub>2</sub> dosing for selected catalysts: (a) Al-Ba1Rh, (b) Al-Ba0.5Rh0.5Pt, (c) 0.5PtAl-Ba0.5Rh, and (d) Al-Ba1Pt. SO<sub>2</sub> reduced the storage capacity of all catalysts and the NO<sub>x</sub> reduction efficiency during fuel rich conditions. Conditions: fuel lean period: 400 ppm NO, 500 ppm C<sub>3</sub>H<sub>6</sub>, 25 ppm SO<sub>2</sub>, and 8% O<sub>2</sub>, balance He. Fuel rich period: 400 ppm NO and 500 ppm C<sub>3</sub>H<sub>6</sub>, 25 ppm SO<sub>2</sub>, balance He. Both at 300 °C and space velocity of 300,000 h<sup>-1</sup>.

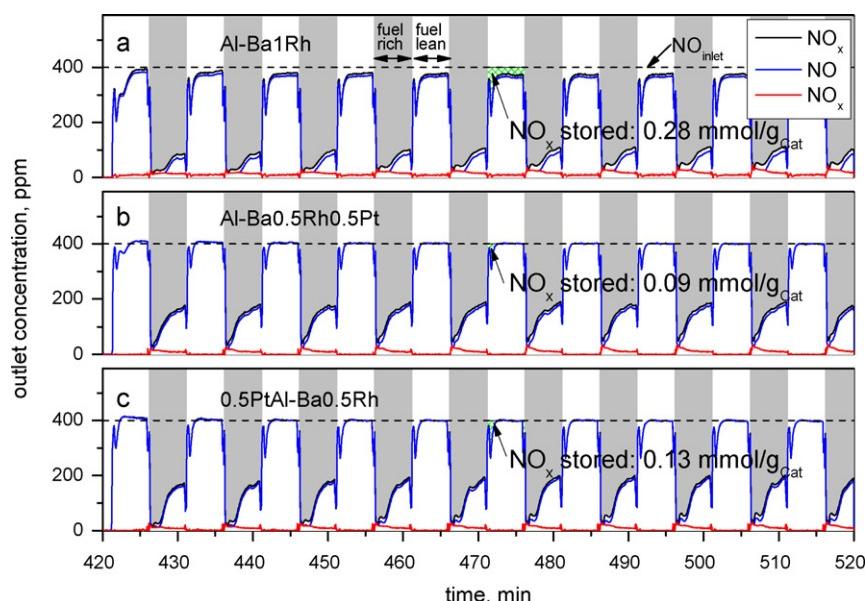


**Fig. 8.** Complete storage and reduction of 0.5PtAl-Ba0.5Rh catalysts in the presence of 25 ppm SO<sub>2</sub>. (a) First 10 min of fuel lean cycle and (b) complete 3 cycles. Conditions: fuel lean period: 400 ppm NO, 500 ppm C<sub>3</sub>H<sub>6</sub>, 25 ppm SO<sub>2</sub>, and 8% O<sub>2</sub>, balance He. Fuel rich period: 400 ppm NO and 500 ppm C<sub>3</sub>H<sub>6</sub>, 25 ppm SO<sub>2</sub>, balance He. Both at 300 °C and space velocity of 300,000 h<sup>-1</sup>.

in the presence of SO<sub>2</sub>. Such an increase of about 20% of the NO<sub>x</sub> storage capacity was already observed for SO<sub>2</sub> exposure during the fuel rich phase [20], although only for one cycle. This effect was explained by the reduction of platinum oxides to metallic platinum by SO<sub>2</sub> [14]. This favors the NO to NO<sub>2</sub> oxidation which enhances NO<sub>x</sub> storage [20].

The *mixed* Rh/Pt on BaCO<sub>3</sub> (Al-Ba0.5Rh0.5Pt, Fig. 7b) also deactivated in the presence of SO<sub>2</sub>. During the fuel rich phase, considerable amount of NO<sub>x</sub> was detected in the reactor outlet stream. The NO<sub>x</sub> reduction activity was reduced and 150 ppm of NO<sub>x</sub> outlet concentration was measured, 2.5 times higher than that for the Rh-only catalyst (Fig. 7a). For Al-Ba0.5Rh0.5Pt the NO<sub>x</sub> storage

ability decreased to 0.10 mmol/g and the NO<sub>x</sub> outlet reached the NO<sub>x inlet</sub> level after the first minute. Compared to the *mixed* Rh/Pt, the *separated* Rh-Pt (0.5PtAl-Ba0.5Rh, Fig. 7c) showed a better performance, although the materials' composition was the same. During fuel rich conditions, not all inlet NO was reduced and an outlet concentration of 110 ppm NO<sub>x</sub> was measured, which was twice that observed with the Rh-only catalyst (Fig. 7a). This can be explained by the contribution of Rh in these catalysts, as for NO<sub>x</sub> reduction Pt deactivates in the presence of SO<sub>2</sub> [21]. The storage capacity was 0.15 mmol/g (Fig. 7c) corresponding to about 45% of that achieved in experiments without addition of 25 ppm SO<sub>2</sub> (Fig. 5b) and more NO<sub>2</sub> was produced compared to Rh-only catalysts



**Fig. 9.** Reactor outlet concentration of NO<sub>x</sub> (NO, NO<sub>2</sub>) with 25 ppm SO<sub>2</sub> after desulfation for selected catalysts: (a) Al-Ba1Rh, (b) Al-Ba0.5Rh0.5Pt, and (c) 0.5PtAl-Ba0.5Rh. The desulfation process did not significantly alter the catalyst performance after the second cycle. Conditions: fuel lean period: 400 ppm NO, 500 ppm C<sub>3</sub>H<sub>6</sub>, 25 ppm SO<sub>2</sub>, and 8% O<sub>2</sub>, balance He. Fuel rich period: 400 ppm NO and 500 ppm C<sub>3</sub>H<sub>6</sub>, 25 ppm SO<sub>2</sub>, balance He. Both at 300 °C and space velocity of 300,000 h<sup>-1</sup>.

(Fig. 7a). A similar effect of Rh was reported by Amberntsson et al. [21], where Pt had a higher NO to NO<sub>2</sub> oxidation activity in the presence of SO<sub>2</sub> than Rh-containing NSR catalysts. As NO<sub>2</sub> is typically stored faster on BaCO<sub>3</sub> [54], the effluent NO<sub>2</sub> is an indication that not enough storage sites (BaCO<sub>3</sub>) were available. Increasing the Ba loading or the BaCO<sub>3</sub> surface could improve NO<sub>x</sub> storage [55].

Fig. 8a shows full storage of NO<sub>x</sub> in the presence of SO<sub>2</sub>, after the *separated* Rh-Pt catalyst was cycled three times (60 min fuel lean and 60 min fuel rich) with NO<sub>x</sub> and SO<sub>2</sub> (Fig. 8b). The storage capacity clearly was reduced with SO<sub>2</sub> dosed over time.

### 3.2.3. NO<sub>x</sub> storage and reduction in the presence of SO<sub>2</sub> after regeneration

Fig. 9 shows the NO<sub>x</sub> outlet concentration *in the presence of SO<sub>2</sub>* after catalysts were desulfated. At elevated temperature the catalyst performance typically decreases as for noble metal sintering and catalyst aging [56]. When comparing the performance before (Fig. 7) and after desulfation (Fig. 9), it becomes evident that the Al-Ba1Rh can be regenerated from sulfur poisoning (for the first cycle), enabling also the evaluation of its stability e.g. if the preferential location was kept or was lost by the sintering process.

The Pt-only catalysts (Al-Ba1Pt (Fig. 7d) and 1PtAl-Ba), that lost their performance in the presence of 25 ppm SO<sub>2</sub>, did not recover to the initial storage capacity (Fig. 10b), only when the catalyst was tested without SO<sub>2</sub> after desulfation (Fig. 10b, series 4) some of the initial NO<sub>x</sub> conversion was recovered. It was therefore not so much the catalysts' thermal aging but the SO<sub>2</sub> poisoning of Pt that limited the performance of these catalysts. Desulfation had a positive effect in the first cycle (Fig. 9), almost all catalysts showed a higher NO<sub>x</sub> conversion in the first cycle after desulfation (series 3) compared prior to desulfation (series 2). During the fuel rich period the content of unreduced NO<sub>x</sub> was the lowest for the Al-Ba1Rh catalyst (100 ppm, Fig. 9a), it increased for *separated* Rh on BaCO<sub>3</sub> and *mixed* Rh/Pt on BaCO<sub>3</sub> (180 ppm, Fig. 9b) and Pt on Al<sub>2</sub>O<sub>3</sub> (160 ppm, Fig. 9c). The highest NO<sub>x</sub> reduction activity for Al-Ba1Rh is attributed to the higher Rh loading. The bimetallic Rh-Pt catalysts had the same Rh loading but the *separated* Rh and Pt had a slightly higher conversion (NO<sub>x</sub> reduction activity) that could be explained by a higher surface area (Al<sub>2</sub>O<sub>3</sub> and BaCO<sub>3</sub>) and higher dispersion (see Table 1), resulting in lower noble metal concentration per surface area making *separated* Rh and Pt less likely to sinter [31] and therefore able to retain a higher NO<sub>x</sub> reduction activity. CO chemisorption measurements after similar heat treatment at 750 °C but without exposure of the catalysts to SO<sub>2</sub> showed a reduced dispersion for catalysts where the noble metal(s) was only deposited on one component, as in Al-Ba1Pt and Al-Ba0.5Rh0.5Pt, where the dispersion (cf. Table 1) decreased to 5.5 and 3.7%, respectively. In contrast, the dispersion of 0.5PtAl-Ba0.5Rh remained constant at 15%.

### 3.2.4. NO<sub>x</sub> conversion of bimetallic catalysts with different Pt and Rh location

Fig. 10 summarizes the NO<sub>x</sub> conversion of all catalysts as a function of cycle number: (1) cycle 1–10, NO<sub>x</sub> conversion without SO<sub>2</sub> exposure, (2) cycle 11–20 NO<sub>x</sub> conversion in the presence of 25 ppm SO<sub>2</sub>. After 20 cycles the catalyst was desulfated at 750 °C and cooled down to 300 °C and subsequently exposed to cycling with 25 ppm SO<sub>2</sub> in the feed (3) cycles 21–30. Note that the inlet conditions of the second and third stages were the same.

Fig. 10a shows that the catalyst with Rh on BaCO<sub>3</sub> (Ba) (circles, Al-Ba1Rh) performed better than the one with Rh on Al<sub>2</sub>O<sub>3</sub> (Al) (triangles, 1RhAl-Ba) in all test series 1–3. Both catalysts showed an increase of the NO<sub>x</sub> conversion, more pronounced with 1RhAl-Ba, with cycle number in the SO<sub>2</sub>-free cycles. Catalyst storage and reduction improved during the first cycles, similar to as-prepared

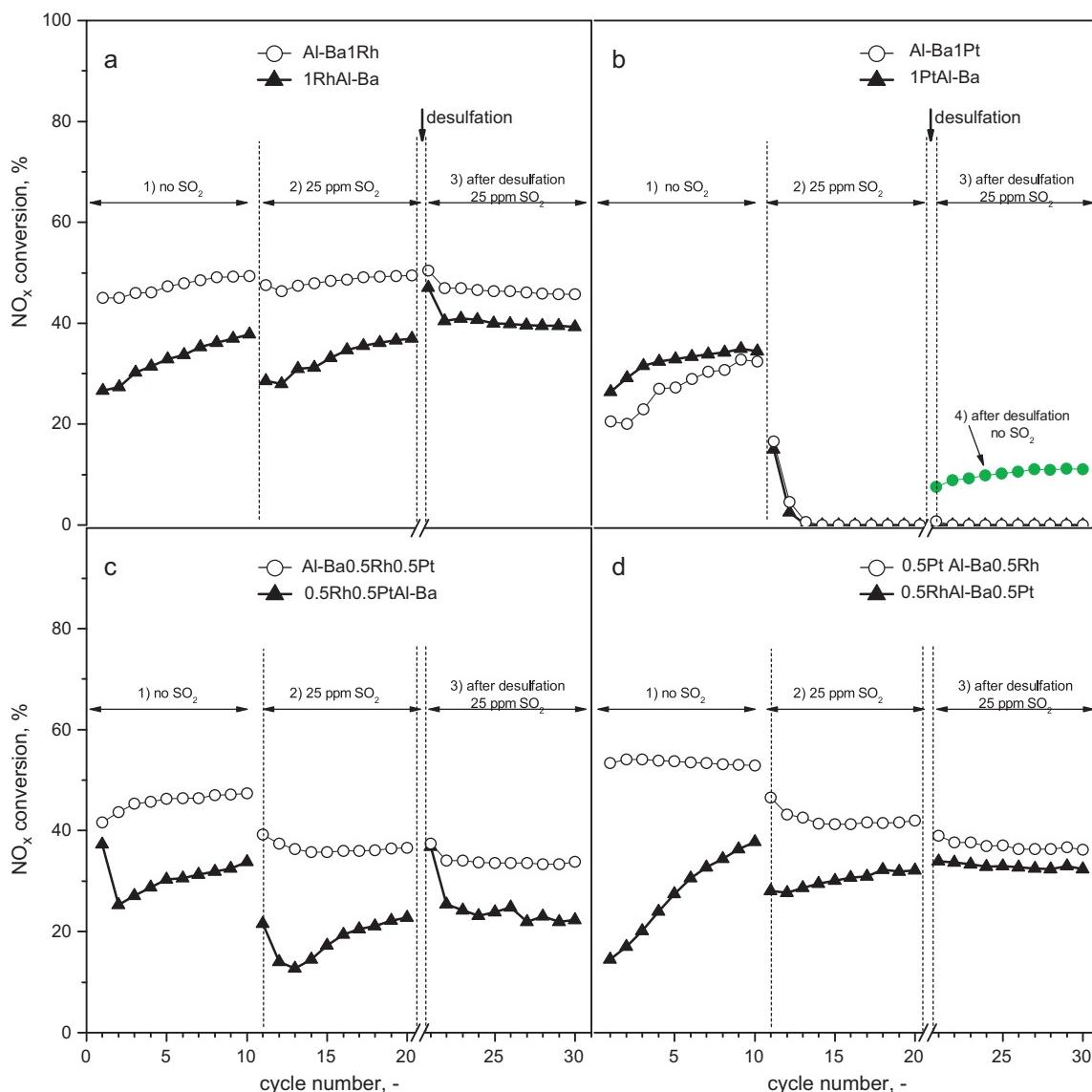
Pt/Ba/Al<sub>2</sub>O<sub>3</sub> catalysts (without reduction before catalytic testing) [36]. In the presence of SO<sub>2</sub> (test series 2, cycles 11–20), the NO<sub>x</sub> conversion first slightly decreased before increasing again (Fig. 10a), indicating that partial poisoning of the noble metal can be beneficial for NO oxidation rate [11]. SO<sub>2</sub> had a stronger influence on the NSR behavior of 1RhAl-Ba but the catalyst regained its performance after 10 cycles (Fig. 10a). After desulfation at 750 °C, there was little difference between both Rh-only catalysts because at high temperature the advantage of preferential deposition of noble metals was lost similarly as previously observed for Pt/K<sub>2</sub>CO<sub>3</sub>/Al<sub>2</sub>O<sub>3</sub> catalysts [57]. This indicates a significant improvement for the 1RhAl-Ba catalysts and a slight loss of activity for Al-Ba1Rh.

Compared to Rh, Pt-only NSR catalysts showed completely different behavior (Fig. 10b). In the absence of SO<sub>2</sub> (series 1), for Pt on Al<sub>2</sub>O<sub>3</sub> (1PtAl-Ba, triangles) a higher NO<sub>x</sub> conversion was observed, as Al-Pt is a highly active catalyst for NO oxidation [34] and NO<sub>2</sub> is stored rapidly on the BaCO<sub>3</sub> [54]. With prolonged cycling, Al-Ba1Pt (circles) increased its performance as NO<sub>x</sub> reduction during the fuel rich period became the limiting step for the overall NSR performance instead of NO oxidation during the fuel lean period. In the presence of SO<sub>2</sub>, however, both catalysts lost their NO<sub>x</sub> conversion activity completely with increasing cycle number. As seen in Fig. 7d, the Pt-only catalysts neither stored nor reduced NO<sub>x</sub> efficiently in the presence of SO<sub>2</sub>. This is in agreement with Amberntsson et al. [21] confirming that Pt is not able to regenerate the catalytic system and therefore NO<sub>x</sub> cannot be stored. Also desulfation of the Pt catalysts (Fig. 10b, series 3) did not increase the NO<sub>x</sub> conversion as the Pt sites were poisoned immediately. Catalytic tests after desulfation without SO<sub>2</sub> in the feed (Fig. 10b, series 4) showed that the catalyst only regained part of its NSR activity, which is attributed to some sintering and/or restructuring during the high temperature desulfation.

When combining both Rh and Pt (Fig. 10c), lower NO<sub>x</sub> conversion was measured compared to the Rh- and Pt-only catalysts (Fig. 10a and b). When Rh and Pt were deposited on BaCO<sub>3</sub> (Al-Ba0.5Rh0.5Pt), the NO<sub>x</sub> conversion was about 40% (circles, Fig. 10c) and decreased to about 30% in the presence of SO<sub>2</sub>. This decrease originates from the loss of NO<sub>x</sub> reduction efficiency during the fuel rich phase (because SO<sub>2</sub> poisons the noble metal) decreasing also the storage capacity (compare Fig. 7b). Also desulfation had relatively little influence on the catalyst performance (cycles 21–30), showing that the catalyst did not deteriorate at the conditions applied. For Rh and Pt on Al<sub>2</sub>O<sub>3</sub> (triangles, 0.5Rh0.5PtAl-Ba), the catalyst performance was unsteady and inferior to that of Rh/Pt on BaCO<sub>3</sub>.

*Separated* Rh and Pt presented in Fig. 10d showed the best performance with Pt on Al<sub>2</sub>O<sub>3</sub> and Rh on BaCO<sub>3</sub> (circles, 0.5PtAl-Ba0.5Rh). This was expected, as NO oxidation on Pt is not limited in the presence of SO<sub>2</sub> while Rh is sulfur-tolerant for NO<sub>x</sub> reduction during fuel rich conditions [21]. Under SO<sub>2</sub>-free conditions, this catalyst showed the best performance while in the presence of SO<sub>2</sub>, NO<sub>x</sub> conversion decreased from 53% to 42% as the reduction activity was partially lost during fuel rich conditions (see Fig. 7c) and the storage capacity on BaCO<sub>3</sub> was lost too (see Figs. 6b and 8b). After desulfation NO<sub>x</sub> conversion decreased to 37% and was therefore slightly lower than for Rh-only catalysts (44%, Fig. 10a). Although it should be reminded that the *separated* Rh/Pt catalysts contained only half of the amount of Rh compared to the Rh-only catalyst (but constant weight loading of noble metals).

The catalytic studies on the flame-made mono- and bimetallic NSR catalysts prepared by controlled deposition of the noble metals on storage and support confirmed that combinations of Rh and Pt can be attractive, as Pt alone did not reduce NO<sub>x</sub> in the presence of SO<sub>2</sub> (Fig. 10b). Rh/Pt mixtures might be considered e.g. when the price of Rh is not extremely high. In 2008 the Rh price had risen



**Fig. 10.**  $\text{NO}_x$  conversion of catalysts during cycling under different conditions at  $300^\circ\text{C}$ : (series 1) in absence of  $\text{SO}_2$ ; (series 2) in presence of  $\text{SO}_2$ ; (series 3) in presence of  $\text{SO}_2$  after desulfation with  $2\% \text{H}_2$  at  $750^\circ\text{C}$ . Monometallic catalysts (a) Rh-only, (b) Pt-only; bimetallic catalysts, (c) mixed Rh/Pt, and (d) separated Rh-Pt. In (b) a catalyst was tested without  $\text{SO}_2$  after the desulfation (series 4).

up to 10,000 US\$/oz,<sup>2</sup> while the current price (2010) for Rh is 2500 US\$/oz, still 47% higher than that of Pt (in 2010 the highest price was 1700 US\$/oz) [58].

Clearly our study indicates that the performance of mono- and bimetallic Rh and Pt catalysts can considerably be improved when noble metals are deposited optimally e.g. Pt on the  $\text{Al}_2\text{O}_3$  support and Rh on the  $\text{BaCO}_3$  storage component. In contrast, lower activity is obtained when Pt and Rh are deposited reversely (Fig. 10d, triangles). In bimetallic catalysts, that is in combinations of Pt with Rh, the sulfur tolerance was always guaranteed, while complete deactivation was observed when Pt-only catalysts were used (Fig. 10b).

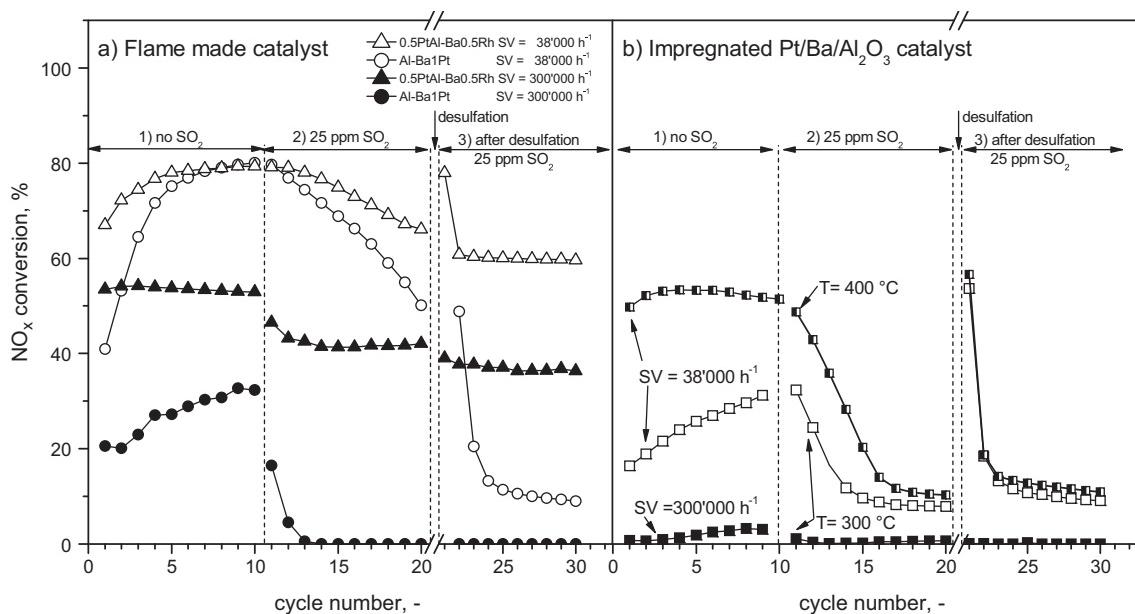
Considering the NSR performance and the metal dispersions determined for the different catalysts (Table 1), no direct correlation is evident, for example Pt-only catalysts exhibited a high dispersion, above 30%, while Rh-only catalysts showed a much lower dispersion but high  $\text{NO}_x$  conversion (Fig. 10a). For combined

Rh/Pt, the catalysts with higher dispersion showed lower  $\text{NO}_x$  conversion in the presence of sulfur, indicating that the effect of the noble metal location had a more prominent effect on the NSR performance than the noble metal dispersion.

### 3.2.5. $\text{NO}_x$ conversion at different space velocity

In order to gain some insight about the behavior of some selected catalysts at lower space velocity (SV), similar series of experiments were performed at SV of  $38,000 \text{ h}^{-1}$ . In Fig. 11a) the performances of two representative catalysts ( $0.5\text{PtAl-Ba}0.5\text{Rh}$  and  $\text{Al-Ba1Pt}$ ) at  $\text{SV} = 38,000 \text{ h}^{-1}$  (open symbols) and  $\text{SV} = 300,000 \text{ h}^{-1}$  (filled symbols) are compared. As expected, at lower SV, the  $\text{NO}_x$  conversion was higher and the time to reach steady state was longer, especially for the series of experiments where  $\text{SO}_2$  was present in the feed. While at  $\text{SV} = 300,000 \text{ h}^{-1}$  steady-state in  $\text{NO}_x$  conversion was reached with  $0.5\text{PtAl-Ba}0.5\text{Rh}$  after 3 cycles at  $\text{SV} = 38,000 \text{ h}^{-1}$ , in the presence of  $\text{SO}_2$ .  $\text{NO}_x$  conversion observed with both catalysts still decreased even after 20 cycles. After desulfation (series 3 in Fig. 11) the observation made in Fig. 10 that Rh is more resistant toward  $\text{SO}_2$  poisoning is corroborated also by the experiments

<sup>2</sup> oz = troy ounce: unit of weight used in noble metal trading. 1 troy ounce  $\approx 31.1 \text{ g}$ .



**Fig. 11.**  $\text{NO}_x$  conversion of selected flame-made catalysts, Al-Ba1Pt and 0.5PtAl-Ba0.5Rh, and impregnated Pt/Ba/Al<sub>2</sub>O<sub>3</sub> reference catalyst during cycling at different space velocities,  $38,000 \text{ h}^{-1}$  (open symbols) and  $300,000 \text{ h}^{-1}$  (full symbols) (a) flame made catalysts Al-Ba1Pt (circle) and 0.5PtAl-Ba0.5Rh (triangles) are compared. In (b) the catalytic performance of the wet-impregnated Pt/Ba/Al<sub>2</sub>O<sub>3</sub> reference catalyst (squares) at the same testing conditions is shown at  $300^\circ\text{C}$  and at  $400^\circ\text{C}$ .

performed at  $38,000 \text{ h}^{-1}$ . The impregnated Pt/Ba/Al<sub>2</sub>O<sub>3</sub> reference catalyst (Fig. 11b) shows similar conversion trends like the flame made catalyst under the different conditions (1–3), albeit at much lower  $\text{NO}_x$  conversion. At high  $\text{SV} = 300,000 \text{ h}^{-1}$  almost no  $\text{NO}_x$  was converted while at  $38,000 \text{ h}^{-1}$  a similar performance like the flame made catalysts at  $300,000 \text{ h}^{-1}$  was observed (compare Fig. 11a and b). Testing the impregnated catalysts at  $400^\circ\text{C}$  resulted in a performance comparable to literature [20], proving the reliability of the testing procedure and the superior performance of the flame made catalysts Al-Ba1Pt compared to the classical wet-impregnated reference catalyst. The main difference between these catalysts is the preferential deposition of the Pt in the flame-made catalyst and the fact that this catalyst is only exposed very shortly to high temperatures in the preparation process while the impregnation catalyst needs annealing at elevated temperatures ( $500^\circ\text{C}$ ) for several hours (5 h) [38]. Interestingly, the superior activity was largely lost after the desulfation at  $750^\circ\text{C}$  (series 3 in Fig. 11a,b) where both the flame-derived and the impregnated Pt/Ba/Al<sub>2</sub>O<sub>3</sub> catalysts showed similar  $\text{NO}_x$  conversion at  $\text{SV} = 38,000 \text{ h}^{-1}$ .

Finally, it should be mentioned that the differences in the catalytic behavior observed for the various catalysts investigated in this study may vary depending on the experimental conditions, such as temperature, type of reductant, duration of lean/reach periods, and space velocity, which in a catalyst bed may lead to different time-dependent chemical and structural gradients [59,60]. Nevertheless, these factors will hardly bias our general conclusion that the preferential deposition of the noble metals either on the storage or support component of mono- and bimetallic catalysts will allow to improve the performance of NSR catalysts.

#### 4. Conclusions

Mono- and bimetallic rhodium and platinum containing NSR catalysts were prepared using a twin nozzle FSP setup allowing preferential deposition of the noble metals on support (Al<sub>2</sub>O<sub>3</sub>) and storage component (BaCO<sub>3</sub>). All catalysts were tested in the presence and absence of SO<sub>2</sub>. CO adsorption combined with DRIFTS revealed significant differences in the vibrational bands

depending on the noble metal and its supporting constituent (Al<sub>2</sub>O<sub>3</sub> or BaCO<sub>3</sub>). While the type of noble metal and the location of its deposition had a strong influence on the NSR efficiency, the effect of the noble metal dispersion was less prominent. Rhodium containing catalysts showed higher  $\text{NO}_x$  conversion as well as a higher resistance toward SO<sub>2</sub> poisoning and relatively little loss of activity upon thermal aging at  $750^\circ\text{C}$ . Combinations of Rh and Pt showed good  $\text{NO}_x$  reduction efficiency especially when Rh was located on BaCO<sub>3</sub>. Best NSR performance was observed with bimetallic catalysts where the noble metals were separated, that is with Pt on Al<sub>2</sub>O<sub>3</sub> and Rh on BaCO<sub>3</sub>.

#### Acknowledgements

We thank Dr. Frank Krumeich (ETH) for STEM/EDXS investigation and the Electron Microscopy Center of ETH Zurich (EMEZ) for providing the necessary infrastructure. We greatly appreciated the financial support by ETH Zürich (TH-09 06-2) and the European Research Council/European Community (under FP7). We thank for the contribution of platinum chemicals by Johnson Matthey PLC.

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